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(54) A curable composition.

(57) A curable composition which provides improved corrosion protection to metals, particularly ferrous metals which are to be exposed to moisture and/or salt, is disclosed. The composition comprises (I) a reaction product (or blend) of a resinous copolymeric siloxane solution with a liquid organohydrogenpolysiloxane, (II) a hydroxy-functional diorganopolysiloxane, (III) a particulate alumina filler and (IV) sufficient catalyst to cure said composition to a non-flowing state.

EP 0 299 641 A2

A CURABLE COMPOSITION

The present invention relates to improved curable compositions. More particularly, the present invention relates to curable silicone coating compositions which provide improved corrosion resistance to metal surfaces, said compositions comprising (I) a liquid copolymeric organopolysiloxane, (II) a polydiorganosiloxane, (III) a particulate alumina filler and (IV) sufficient catalyst to cure said compositions.

5 In United States Patent No. 4,322,518, assigned to the assignee of the present invention, Blizzard discloses silicone coating compositions which comprise a solventless liquid copolymeric organopolysiloxane comprising a curable silicone polymer fluid or gum and a liquid SiO₂-based resin as the sole curing agent for the fluid or gum. When cured on various substrates, these silicone compositions provide release coatings having controllable release forces for adhesives adhered thereto.

10 Blizzard and Swihart, in United States Patent No. 4,537,829, assigned to the assignee of the present invention, teach compositions similar to those described by Blizzard, cited supra. In addition to the curable silicone polymer and liquid SiO₂-based resin, these compositions further comprise an organosilicon resin consisting essentially of dimethylvinylsiloxyl units, trimethylsiloxyl units and SiO_{4/2} units and a hydrosilylation catalyst. These compositions, when cured, provided improved resistance to fuels and a high degree of 15 corrosion protection to metal substrates.

20 It has now been found that certain compositions prepared according to the disclosures of Blizzard, cited supra, provide improved corrosion protection to metals, particularly ferrous metals, when cured on the surfaces thereof. It has also been discovered that the incorporation of up to about 50% by weight of alumina or hydrated alumina in these compositions further augments the corrosion resistance of metals coated with 25 the cured compositions. Surprisingly, incorporation of like proportions of hydrated alumina in the compositions taught by Blizzard and Swihart, cited supra, did not result in such improvements.

The present invention therefore relates to a composition comprising:

25 (I) from about 1 to 99 parts by weight of a liquid organopolysiloxane copolymer, prepared by a method comprising (A) forming a homogeneous mixture having an acid number greater than zero and consisting essentially of (a) an organic solvent solution of a resinous copolymeric siloxane containing silicon-bonded hydroxyl radicals and consisting essentially of R₃SiO_{1/2} units and SiO_{4/2} units wherein the ratio of R₃SiO_{1/2} units to SiO_{4/2} units is 0.6:1 to 0.9:1 and each R denotes, independently, a monovalent hydrocarbon radical and (b) a liquid organohydrogenpolysiloxane wherein each organic radical is, 30 independently, a monovalent hydrocarbon radical, there being an average of at least one silicon-bonded hydrogen radical per molecule of said organohydrogenpolysiloxane, and (B) heating said homogeneous mixture to remove substantially all of said organic solvent therefrom;

(II) from about 99 to 1 parts by weight of a hydroxy-functional diorganopolysiloxane having the average formula (HO)Rⁿ₂SiO(Rⁿ₂SiO)_cSiRⁿ₂(OH) wherein Rⁿ is a group independently selected from alkyl, cycloalkyl, haloalkyl, aromatic or haloaromatic radicals and c has a value sufficient to provide a viscosity of 35 about 1 to 1,000,000 Poise at 25°C. for the diorganopolysiloxane;

(III) from about 1 to 100 parts by weight, per 100 parts of said component (I) plus component (II), of a particulate filler selected from alumina, alumina monohydrate or alumina trihydrate; and

(IV) sufficient catalyst to cure said composition to a non-flowing state.

This invention further relates to a similar composition to that described above, wherein said component 40 (I) is prepared by simply mixing said components (a) and (b) without subsequent heating and removal of solvent therefrom.

This invention still further relates to a method of coating a metal substrate with either of the above described compositions and subsequently curing said composition to a non-flowing state.

45 Component (I) of the compositions of this invention is a liquid copolymeric organopolysiloxane. It may be prepared by reacting (a) a resinous copolymeric siloxane with (b) a liquid organohydrogenpolysiloxane. Alternatively, component (I) may be prepared by simply blending reactants (a) and (b) and using this mixture directly in the compositions of the present invention.

50 Component (a) that is used to prepare the liquid copolymeric organopolysiloxane (I) is an organic solvent solution of a resinous copolymeric siloxane which consists essentially of R₃SiO_{1/2} siloxane units and SiO_{4/2} siloxane units in a molar ratio which provides from 0.6 to 0.9 R₃SiO_{1/2} units for every SiO_{4/2} unit. Each R denotes a monovalent hydrocarbon radical; such as an alkyl radical, such as methyl, ethyl, isopropyl, butyl and hexyl; an alkenyl radical, such as vinyl and allyl; and aryl radical, such as phenyl, tolyl and xylyl; an arylalkyl radical, such as beta-phenylethyl and beta-phenylpropyl; and a cycloaliphatic radical, such as cyclopentyl, and cyclohexyl. Preferably, all R radicals in component (a) are lower alkyl radicals although a minor portion of them can be replaced with other monovalent hydrocarbon radicals such as the

v vinyl radical and/or phenyl radical to provide additional properties for the resinous copolymer such as the reactivity attendant therewith.

In a preferred curable coating composition of this invention the resinous copolymeric siloxane portion of component (a) consists essentially of $(CH_3)_3SiO_{1/2}$ siloxane units and $SiO_{4/2}$ siloxane units, in the molar ratio of about 0.75:1.

Resinous copolymeric siloxanes consisting of $R_3SiO_{1/2}$ units and $SiO_{4/2}$ units are well known in the art and are described by, for example, Daudt et al., U.S. Patent No. 2,676,182.

Resinous copolymeric siloxanes are typically prepared in an organic solvent which can conveniently serve as the organic solvent portion of component (a). The particular organic solvent portion of component

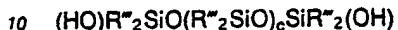
(a) is not critical and can be, for example, an aliphatic hydrocarbon, an aromatic hydrocarbon or halogenated derivatives of either, or mixtures thereof. Particularly useful organic solvents include benzene, toluene, xylene, trichloroethylene and mineral spirits.

bonded hydrogen radicals which provide chemical reactivity therefor in the compositions of this invention.

Further details dealing with the preparation of component (I) by this method, as well as descriptions of components (a) and (b), may be found in U.S. Patent No. 4,322,518, cited supra.

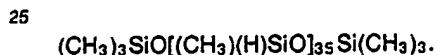
When component (I) is a room temperature blend of components (a) and (b), its preparation simply consists of forming a homogeneous solution between these ingredients. As in the case of the reaction product, described above, an acid number greater than zero is required and an acid number between about 0.1 and 1, on a solids basis, is preferred.

Component (II) of this invention is a polydiorganosiloxane having the general formula



wherein R'' denotes a monovalent hydrocarbon radical independently selected from the group of R radicals indicated above for component (I). For the purpose of this invention, at least 95 percent of the R'' radicals are methyl (Me) and it is preferred that all R'' radicals are methyl. Herein, c has an average value which is sufficient to provide a viscosity for component (II) of about 1 to 1,000,000 Poise at 25°C. Preferably, the viscosity of component (II) is about 200,000 Poise at 25°C. and this component is ordinarily dissolved in a solvent, such as toluene, xylene, naptha spirits, VMP naptha, low molecular weight ketones or hexane, before combining with components (I) and (III) of this invention.

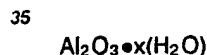
A highly preferred component (II) is a mixture of (1) about 7 parts by weight of a hydroxyl endblocked polydimethylsiloxane having an approximate average molecular weight of 40,000 which contains less than about 2 weight percent of a mixture of cyclic polydimethylsiloxanes having a degree of polymerization ranging from 3 to 40 with (2) 1 part of a silanol-ended polydimethylsiloxane gum having a viscosity of about 100,000 Poise at 25°C. and containing about 1% pyrogenic silica and 1 part of the liquid organohydrogen-polysiloxane



As noted above, this preferred component (II) is ordinarily added in the form of a solution in forming the compositions of this invention.

30 Polydiorganosiloxanes which are suitable for use as component (II) are well known in the art and many of these fluids or gums are available commercially. Therefore, further description of methods for the preparation of such materials is not detailed herein.

Component (III) of the present invention is a particulate alumina or hydrated alumina having the general formula



wherein x is 0, 1 or 3. It is preferred that this filler have a uniform particle size and an average diameter of about 1 micron or less. Most preferably, component (III) is alumina trihydrate (i.e., x = 3) having a uniform particle diameter averaging about 1 micron.

The alumina fillers or component (III) are well known in the art and are commercially available, hence further description of methods of preparation will not be addressed herein.

45 Component (IV) of the present invention is a curing amount of a curing catalyst. Catalysts suitable for use in this invention include any of the compounds which are known to facilitate the condensation reactions between SiOH groups and between SiOH and SiH groups. For example, the catalysts contemplated may be salts of heavy metals, such as dibutyltin diacetate and stannous octoate. These catalysts, and their use in promoting the above-mentioned reactions, are well known in the art.

The compositions of this invention can further comprise typical silicone adjuvants such as catalysts, fillers, pigments, dyes and cure-control additives, if desired.

50 The compositions of this invention are prepared by thoroughly mixing, on a solids basis, from about 1 to 99 parts by weight, preferably from 15 to 25 parts, of component (I), from about 99 to 1 parts by weight, preferably from 85 to 75 parts, of component (II) and, based on 100 parts by weight of component (I) plus component (II), from about 1 to 100 parts by weight of component (III). This corresponds to an alumina (or alumina hydrate) content of about 0.5 to about 50 weight percent based on total silicone polymer content. It is preferred that component (III) is employed in the range of about 10 to 80 parts by weight based on 100 parts (solids basis) of component (I) plus component (II). It has been found that when much more than approximately 100 parts of the alumina filler per 100 parts of total silicone polymer is used (e.g., about 150 parts per 100 parts of I plus II), the resultant coatings are inferior in that filler particles on the surface are not

completely coated with the silicone components and such compositions tend to be abrasive and weak. This has been observed in Taber abrasion measurements wherein such highly filled coatings are readily worn down. On the other hand, compositions containing as high a level of alumina trihydrate as is consistent with corrosion protection characteristics benefit from the reduced cost and improved fire retardancy imparted by this filler.

In highly preferred compositions of the present invention, about 21 parts by weight of the preferred devolatilized reaction product, described supra as component (I), is combined with about 79 parts by weight of the preferred component (II), each being measured on a solids basis. The preferred filler (component III), alumina trihydrate, is incorporated at about 17 to about 67 parts by weight per 100 parts of total solids of components (I) plus (II). These embodiments are catalyzed with approximately 5% of dibutyltin diacetate, based on the total solids of components (I) and (II).

Any of the high shear mixers commonly employed in the art may be used to disperse the filler. Examples of such mixers include Ross, Jiffy and Meyers mixtures. As far as is known, the order of mixing is not critical to the operability of this invention as long as the filler is thoroughly dispersed in components (I) and (II). It is preferred, however, to first disperse the filler (component III) in component (II) and then to mix in component (I), again using high shear to obtain a good dispersion. It is further preferred to pre-treat the alumina filler with a portion (typically about 2%) of component (I) before mixing this with the rest of component (I) and component (II). This pre-treatment may be carried out, for example, by rolling the filler, the portion of component (I) and an inert, volatile organic solvent for (I) in a ball mill. After rolling, the treated filler dispersion is dried to remove the solvent before forming the compositions of this invention.

Sufficient catalyst (component IV) to allow cure of the composition to a non-flowing state is generally added just before the compositions are to be used (cured). In this connection, it has been found that even when the compositions are not catalyzed they should not be allowed to age for long periods before using. Thus, it was observed that coatings formed from such compositions which are aged at room temperature for one week before being catalyzed, coated onto steel panels and cured thereon, were inferior to those prepared from fresh compositions. It is, therefore, preferred to store the compositions of the present invention as three separate components, to be mixed just before use: (1) filler (i.e., component III) dispersed in component (II), (2) component (I) and (3) catalyst. Of course, solvent may be added to any of these for handling convenience.

The compositions of the present invention may be employed in electronic applications, such as circuit board coatings and conformal coatings, or for the fabrication of gaskets to be used in connecting dissimilar metals. They find particular utility as protective coating compositions for metal substrates. When applied as 100% solids or from solution and cured on such substrates as iron, steel, aluminum, brass or copper, coatings comprising these compositions provide improved corrosion protection to the substrates. This is particularly true for the case of ferrous metals exposed to moisture and salt.

To form such coating compositions, the compositions of this invention are typically diluted with a sufficient quantity of a good solvent for components (I) and (II) in order to provide a desired coating composition viscosity. Such solvents as hexane, heptane, toluene, xylene, mineral spirits or ketones are suitable for this purpose, xylene being preferred. Alternatively, a 100% solids system is also contemplated herein, particularly when component (II) has a low viscosity.

The coating compositions of this invention may be applied to metal surfaces by any of the methods commonly practiced in the coating arts. For example, substrates may be dipped, brushed, sprayed or flow coated. Optimal amounts of solvent and catalyst to be included in such coating compositions may readily be determined by routine experimentation.

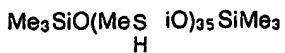
After coating of the metal substrates with the coating compositions of this invention, the coatings, which typically are at least about 1 mil in thickness, are cured, preferably at elevated temperatures such as 125 to 150 °C. Alternatively, when sufficient catalyst is used, the compositions of the present invention can be cured at room temperature.

The following examples are presented to further illustrate the compositions of this invention, but are not to be construed as limiting the invention, which is delineated in the appended claims. All parts and percentages in the examples are on a weight basis unless indicated to the contrary and viscosities are measured at 25 °C.

The following components were used to prepare the compositions of this invention.

FLUID A - A 70% xylene solution of a siloxane resin copolymer consisting essentially of $(CH_3)_3SiO_{1/2}$ units and $SiO_{4/2}$ units in a molar ratio of approximately 0.75:1.

FLUID B - A liquid organohydrogenpolysiloxane having the average formula



wherein M denotes the methyl radical.

FLUID C - A liquid organopolysiloxane copolymer was prepared according to the methods of United States Patent No. 4,310,678 wherein 59 parts of FLUID A was thoroughly mixed with 41 parts of FLUID B using a nitrogen purge. Xylene solvent was removed as this mixture was heated under a vacuum of about 100 mm Hg at 150 °C. for 2 hours to yield a reaction product containing a 1:1 weight ratio of the siloxane resin copolymer to the organohydrogenpolysiloxane.

FLUID D - A solution consisting of 34 parts of a silanol-ended polydimethylsiloxane gum having a viscosity of about 100,000 Poise and containing about 1% pyrogenic silica, 1 part of the liquid organohydrogenpolysiloxane used in FLUID B and 65 parts of xylene, was prepared.

FLUID E - A hydroxy-endblocked polydimethylsiloxane having an approximate number average molecular weight of 40,000 which contained less than 2 weight percent of a mixture of dimethylcyclopolsiloxanes having a degree of polymerization ranging from 3 to 40.

ATH- A precipitated alumina trihydrate filler having a uniform average particle size of approximately one micron in diameter and obtained from the Aluminum Company of America (Pittsburgh, PA) under the trade name HYDRAL 710.

In the following examples, component (II) of the compositions of the present invention comprises a mixture of the hydroxyl-functional polydimethylsiloxanes of FLUID D and FLUID E.

20

Examples 1 - 3

These examples illustrate the effect of varying the ATH content of the compositions of the present invention. In these examples component (I) is FLUID C, a devolatilized reaction product of FLUID A and FLUID B. On a solids basis, the ratio of component (II) to component (I) employed in Examples 1-3 was about 86:14.

Proportions of the components of Examples 1 and 2 are shown in Table 1, below. The mixing procedure consisted of first preparing a treated ATH (alumina trihydrate). A mixture of 1 gram of FLUID C, 210 grams of hexane and 50 grams of ATH was rolled in a polyethylene jar containing 1:2 inch ceramic pebbles for about 24 hours. The hexane solvent was then removed from this combination by drying the filler at room temperature followed by heating at 150 °C. for 1/2 hour, to form the treated ATH used in these compositions. This pre-treated ATH was mixed with FLUID D and FLUID E (i.e., component II) in a JIFFY high shear mixer till a uniform dispersion resulted. FLUID C was then added and mixed in at high shear. A similar composition, but without the alumina trihydrate filler, was prepared by simply stirring components (I) and (II) together to obtain a homogenous solution, shown in Table 1 as (Comparative) Example 3. At this point, the calculated alumina trihydrate contents (solids basis) of the compositions of Example 1 and Example 2 were 18 and 67 parts ATH per 100 parts of component (I) plus component (II), respectively (15% and 40%, respectively).

The above described ingredients were combined with additional xylene solvent (to provide a flowable consistency for subsequent coating of steel panels) and catalyzed with 5 percent (based on total silicone content) of dibutyltindiacetate (DBTDA) to form the compositions of this invention, as shown in Table 1.

Table 1

45

	Grams ATH	Grams FLUID C	Grams FLUID D	Grams FLUID E	Grams Xylene	Grams DBTDA
Ex. 1	10.0	8.0	17.6	42.5	17.4	2.8
Ex. 2	21.4	4.5	9.3	24.1	30.1	1.6
(Comparative) Ex. 3	---	6.2	12.0	31.3	10.1	2.1

55 The catalyzed compositions of Examples 1 - 3 were coated onto pre-cleaned cold-rolled steel panels using a 6 mil wet gap draw down bar. The resulting coatings were allowed to partially cure at room temperature (R.T.) for about 15 - 60 minutes, till they were tack-free, and were then further cured in an air oven at 150 °C. for 5 minutes. Cured film thicknesses ranged from 0.6 to 0.9 mil.

Corrosion resistance was evaluated by ASTM test method D1654, wherein a 2 inch-long scribe line was

cut in each coated panel to expose a fine line of bare metal. The scribed panels were then subjected to salt spray (fog) testing according to ASTM test method B117, using a sodium chloride concentration of 2.5% at a temperature of 35°C. Before placing the coated panels in the salt spray apparatus, the edges of each panel were covered with Mylar pressure-sensitive tape which was then further sealed with paraffin wax in order to eliminate edge corrosion effects. After being exposed for the times indicated in Table 2, below, the panels were rinsed with water and then evaluated.

Results showing average corrosion "creep" at the scribe line after various exposure times are reported in Table 2, below. In this table, a rating of 10 represents zero creep (i.e., initial rating before exposure) and a rating of 0 represents greater than a 5/8 inch (greater than 16 mm) scribe creep, wherein the scribe creep is defined as the average perpendicular distance from the scribe line where rust was detected. There was no surface rusting, staining or blistering observed on any of the panels in the non-scribed areas (i.e., a surface rust rating of 10 for all samples according to ASTM test method D610). Results of these measurements indicate that the coatings based on the compositions of this invention exhibit significantly less scribe creep than the control formulation having no aluminum trihydrate filler and are, therefore, more resistant to corrosion.

Table 2

	Coating Composition	Creep Rating per ASTM D1654			
		48 hr	120 hr	288 hr	1,266 hr
	Example 1	9	7	5	5
	Example 2	9	8	6	5
	(Comparative) Example 3	8	4	2	1

In addition to the above evaluation, the amount of "undercutting" of each coating was observed as a function of salt spray exposure time. While the panels were still wet from the salt spray chamber, the amount of "undercutting" was measured by gently probing the surface of each panel with a spatula tip to determine the farthest point from the end of the scribe line at which the coating had delaminated (separated) from the steel substrate (i.e., where either movement of the coating or color change could be detected). The boundary so defined represents an unprotected area, beyond that delineated by the above described rust creep, wherein the substrate is more vulnerable to corrosion than where the coating is firmly adhered to the substrate. Results of these measurements (Table 3) indicate that the coatings based on the compositions of this invention exhibit significantly less undercutting than the control formulation having no alumina trihydrate filler and are, therefore, less susceptible to further corrosion.

Table 3

	Coating Composition	Maximum Extent of Undercutting After Salt Spray Exposure (inches)				
		348 hr	552 hr	690 hr	1,026 hr	1,266 hr
	Example 1	3/32	1/8	1/8	1/4	3/16 - 1/4
	Example 2	1/16	1/8	3/16	1/8	1/8 - 1/4
	(Comparative) Example 3	7/16	5/8	5/8	7/8	---

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Examples 4 - 7

The following examples illustrate the effect of varying the ratio of component (II) to component (I) at a constant ATH level in the compositions of the present invention. Mixing procedures similar to those described in Examples 1 and 2 were followed except that the ATH was not pre-treated. These compositions, which each contained 67 parts ATH per 100 parts of component (I) plus component (II) (40% ATH) on a solids basis before being catalyzed, are shown in Table 4, below. In Examples 4, 5 and 6, the ratio of

component (II) to component (I), on a solids basis, was calculated as 93:7, 86:14 and 79:21, respectively. For comparison, a composition containing no ATH, (Comparative) Example 7, was prepared in the manner described in (Comparative) Example 3, above, wherein the ratio of component (II) to component (I) was again 86:14. These compositions were diluted with xylene and catalyzed with DBTDA, as shown in Table 4 below, just before coating test panels.

Table 4

	Grams ATH	Grams FLUID C	Grams FLUID D	Grams FLUID E	Grams Xylene	Grams DBTDA
Ex. 4	136.0	14.5	64.0	167.0	192.0	10.0
Ex. 5	136.0	29.0	59.0	154.0	192.0	10.0
Ex. 6	136.0	43.4	54.1	141.1	192.0	10.0
(Comparative) Ex. 7	---	29.0	59.0	154.0	30.0	10.0

Examples 8 - 10

These examples illustrate the use of cold-blended (i.e., unreacted) component (I) with various levels of ATH to form the compositions of the present invention. In these examples, the ATH was not pre-treated but was otherwise dispersed in component (II) as above. A blend of FLUID A and FLUID B (i.e., component I), having a solids basis ratio of 1:1 of the siloxane resin copolymer to the organohydrogenpolysiloxane, was added to this dispersion as shown in Table 5, below. Additionally, (Comparison) Example 10 containing no ATH was prepared by stirring components (I) and (II) together as in previous comparison examples. Each of these examples had a calculated ratio of component (II) to component (I), on a solids basis, of about 86:14. The calculated ATH contents (solids basis, before catalyst addition) of Examples 8 and 9 were 17 and 67 parts ATH per 100 parts of component (I) plus component (II), respectively (15% and 40%, respectively). As before, xylene and catalyst were added to each composition just before coating test panels.

Table 5

	Composition	Grams ATH	Grams FLUID A	Grams FLUID B	Grams FLUID D	Grams Fluid E	Grams Xylene	Grams DBTDA
Ex. 8	35.4	20.7	14.5	59.0	154.0	63.0	10.0	
Ex. 9	136.0	20.7	14.5	59.0	154.0	192.0	10.0	
(Comparative) Ex. 10	---	20.7	14.5	59.0	154.0	30.0	10.0	

The compositions of Examples 4 - 10 were coated onto cold-rolled steel panels, as described above, and were allowed to air-cure for 7 days at room temperature, after which they were further cured for 20 minutes at 149 °C. The coatings were subjected to salt spray exposure, as above, after an "X" was scribed in the cured film per ASTM test method D1654. Table 6 shows observed scribe creep ratings (10 = initial rating) after 288 hours of exposure. Also shown is the surface rust rating (10 = initial rating) according to ASTM D610.

Table 6

Creep Ratings per ASTM D1654				
	Composition	Dry Film Thickness (mil)	Creep Rating	Surface Rust Rating
5	Ex. 4	0.7	4	10
10	Ex. 5	0.65	6	10
15	Ex. 6	0.7	6.5	10
20	(Comparative) Ex. 7	0.7	0	9
25	Ex. 8	0.7	5.5	9.5
30	Ex. 9	0.75	5	9.5
35	(Comparative) Ex. 10	0.75	1	8.5

It can be seen that the compositions of the present invention provide improved corrosion protection to the steel substrates relative to compositions containing no ATH.

When coatings containing comparable amounts of ATH dispersed in silicone compositions taught by Blizzard and Swihart, U.S. Patent No. 4,537,829, cited supra, were evaluated after 288 hours of salt spray exposure, it was found that these lacked the excellent undercutting characteristics of the compositions of the present invention. After about 1000 hours of exposure, these comparative systems also displayed considerably more scribe creep than the compositions of the present invention.

Claims

1. A curable composition comprising:

(I) from about 1 to 99 parts by weight of a liquid organopolysiloxane copolymer, prepared by a method comprising (A) forming a homogeneous mixture having an acid number greater than zero and consisting essentially of (a) an organic solvent solution of a resinous copolymeric siloxane containing silicon-bonded hydroxyl radicals and consisting essentially of $R_3SiO_{1/2}$ units and $SiO_{4/2}$ units wherein the ratio of $R_3SiO_{1/2}$ units to $SiO_{4/2}$ units is 0.6:1 to 0.9:1 and each R denotes, independently, a monovalent hydrocarbon radical and (b) a liquid organohydrogenpolysiloxane wherein each organic radical is, independently, a monovalent hydrocarbon radical, there being an average of at least one silicon-bonded hydrogen radical per molecule of said organohydrogenpolysiloxane, and (B) heating said homogeneous mixture to remove substantially all of said organic solvent therefrom;

(II) from about 99 to 1 parts by weight of a hydroxy-functional diorganopolysiloxane having the average formula $(HO)R''_2SiO(R''_2SiO)_cSiR''_2(OH)$ wherein R'' is a group independently selected from alkyl, cycloalkyl, haloalkyl, aromatic or haloaromatic radicals and c has a value sufficient to provide a viscosity of about 1 to 1,000,000 Poise at 25°C. for the diorganopolysiloxane;

(III) from about 1 to 100 parts by weight, per 100 parts of said component (I) plus component (II), of a particulate filler selected from alumina, alumina monohydrate or alumina trihydrate; and

(IV) sufficient catalyst to cure said composition to a non-flowing state.

2. A curable composition comprising:

(I) from about 1 to 99 parts by weight, on a solids basis, or a liquid organopolysiloxane copolymer, prepared by a method comprising forming a homogeneous mixture having an acid number greater than zero and consisting essentially of (a) an organic solvent solution of a resinous copolymeric siloxane containing silicon-bonded hydroxyl radicals and consisting essentially of $R_3SiO_{1/2}$ units and $SiO_{4/2}$ units wherein the ratio of $R_3SiO_{1/2}$ units to $SiO_{4/2}$ units is 0.6:1 to 0.9:1 and each R denotes, independently, a monovalent hydrocarbon radical and (b) a liquid organohydrogenpolysiloxane wherein each organic radical is, independently, a monovalent hydro-carbon radical, there being an average of at least one silicon-bonded hydrogen radical per molecule of said organohydrogenpolysiloxane;

(II) from about 99 to 1 parts by weight of a hydroxy-functional diorganopolysiloxane having the average formula $(HO)R''_2SiO(R''_2SiO)_cSiR''_2(OH)$ wherein R'' is a group independently selected from alkyl, cycloalkyl, haloalkyl, aromatic or haloaromatic radicals and c has a value sufficient to provide a viscosity of about 1 to 1,000,000 Poise at 25°C. for the diorganopolysiloxane;

(III) from about 1 to 100 parts by weight, per 100 parts of said component (I) plus component (II), of a particulate filler selected from alumina, alumina monohydrate or alumina trihydrate; and
(IV) sufficient catalyst to cure said composition to a non-flowing state.

3. A metal substrate bearing the cured composition of claim 1.

5 4. A method of coating a metal substrate with a curable composition and subsequently curing said composition to a non-flowing state, characterised in that the composition of claim 1 is used as said curable composition.

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(54) A curable composition.

(57) A curable composition which provides improved corrosion protection to metals, particularly ferrous metals which are to be exposed to moisture and/or salt, is disclosed. The composition comprises (I) a reaction product (or blend) of a resinous copolymeric siloxane solution with a liquid organohydrogen-polysiloxane, (II) a hydroxy-functional diorganopolysiloxane, (III) a particulate alumina filler and (IV) sufficient catalyst to cure said composition to a non-flowing state.

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EUROPEAN SEARCH REPORT

Application Number

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DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl.4)
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.4)
Y,D	US-A-4 537 829 (BLIZZARD et al.) * Claims 1-7,12-17,22-27; column 5, lines 53-57; column 6, lines 47-64 * ---	1-4	C 09 D 3/82 C 08 K 3/22 C 08 L 83/10
Y,D	US-A-4 322 518 (BLIZZARD) * Claims 1-7,9,12,14; column 7, lines 7-27 * ---	1-4	
Y	US-A-4 450 255 (BANEY) * Claims; column 3, lines 10-21 * ---	1-4	
A	US-A-4 460 712 (BLIZZARD et al.) * Claims 1,6,7; column 6, line 65 - column 7, line 30 * ---	1-4	
A	PATENT ABSTRACTS OF JAPAN, vol. 11, no. 214 (C-434)[2661], 10th July 1987; & JP-A-62 32 157 (YOSHIO ICHIKAWA) 12-02-1987 ---	1-4	
A	WPI, FILE SUPPLIER, accession no. 78-03354A, Derwent Publications Ltd, London, GB; & JP-A-52 141 861 (HITACHI K.K.) 26-11-1977 * Abstract * ---	1,2	TECHNICAL FIELDS SEARCHED (Int. Cl.4)
A	US-A-3 965 065 (ELLIOTT) * Claims; column 3, lines 20-25 * -----	1,2	C 09 D C 08 K C 08 L
The present search report has been drawn up for all claims			
Place of search	Date of completion of the search	Examiner	
THE HAGUE	22-06-1990	HOLLENDER C.J.F.	
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	
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